REPORT DOCUMENTATION PAGE

Form Approved OMB No. 0704-0188

The public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing the burden, to Department of Defense, Washington Headquarters Services, Directorate for Information Operations and Reports (0704-0188), 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 2202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any person that the collection of information if it does not display a currently valid OMR control number.

			t does not display a currently va IE ABOVE ADDRESS.	lid OMB control nur	nber.				
1. REPORT DATE (DD-MM-YYYY) 2. REPORT TYPE			RT TYPE			3. DATES COVERED (From - To)			
	tember 2008		Journal Arti	icle		November, December, 2008			
4. TITLE AND	SUBTITLE				5a. CO	NTRACT NUMBER			
		redict physiolo	gical status from ambi	ent					
environment a	and heart rate.				5b. GRANT NUMBER				
					E. DDC	OCDANA ELENACIT NUINADED			
					SC. PRO	OGRAM ELEMENT NUMBER			
6. AUTHOR(S)					5d. PROJECT NUMBER				
Miyo Yokota, Larry Berglund, Samuel Cheuvront, William Santee, William						5e. TASK NUMBER			
Latzka, Scott Montain, Margaret Kolka, Daniel Moran.									
					5f. WORK UNIT NUMBER				
7. PERFORMIN	IG ORGANIZATI	ON NAME(S) AN	ID ADDRESS(ES)			8. PERFORMING ORGANIZATION			
	d Biomedical I				REPORT NUMBER				
						M06-30			
U.S. Army Research Institute of Environmental Medicine Building 42 - Kansas Street									
Natick, MA 0									
9. SPONSORIN	IG/MONITORING	AGENCY NAM	E(S) AND ADDRESS(ES)			10. SPONSOR/MONITOR'S ACRONYM(S)			
U.S. Army Mo	edical Research	and Materiel	Command						
Fort Detrick, I									
					11. SPONSOR/MONITOR'S REPORT				
						NUMBER(S)			
12. DISTRIBUT	ION/AVAILABILI	TY STATEMENT	Ī						
Approved for	public release;	distribution un	limited						
12 CUDDIEME	NTARY NOTES								
13. SUPPLEME	NIAKY NOTES								
14. ABSTRACT	•								
		, model wee de	valanad for pradicting	raal tima nhi	raiologia	al responses of workers engaged in various			
tasks for	ermoregulatory	moder was de	veroped for predicting	rear-time pmy	siologica	ar responses of workers engaged in various			
	e. The unique t	eature of the p	resent model is primar	ilv on metabo	lic activi	ity inputs derived from minimum			
						ndividual anthropological characteristics			
						was validated using data from five			
laboratory stu	dies $(n = 63)$ w	ith varied envi	ronments, clothing, and	d heat acclima	ation stat	us. Overall, Tc predictions using this			
simplified model, corresponded well with measured values (root mean square deviation: 0.05–0.31 °C).									
Published by l	Elsevier Ltd.								
15. SUBJECT T	ERMS								
Real-time mod	deling: Heat str	ess: Heart rate:	Core temperature; Air	r temperature.					
	g, 110ac st.	055, 110410 1400,	, core temperature, rin	· · · · · · · · · · · · · · · · · · ·					
16. SECURITY CLASSIFICATION OF: 17. LIMITATION OF 18. NUMBER					R 19a. NAME OF RESPONSIBLE PERSON				
a. REPORT	b. ABSTRACT	c. THIS PAGE	ABSTRACT	OF PAGES					
Unclassified	Unclassified	Unclassified	Unclassified	8	19b. TEL	b. TELEPHONE NUMBER (Include area code)			



Computers in Biology and Medicine 38 (2008) 1187-1193

Computers in Biology and Medicine

www.intl.elsevierhealth.com/journals/cobm

Thermoregulatory model to predict physiological status from ambient environment and heart rate

Miyo Yokota^{a,*}, Larry Berglund^a, Samuel Cheuvront^a, William Santee^a, William Latzka^a, Scott Montain^a, Margaret Kolka^a, Daniel Moran^b

^aBiophysics and Biomedical Modeling Division, US Army Research Institute of Environmental Medicine (USARIEM), Kansas Street, Bldg 42, Natick, MA 01760-5007, USA

^bHeller Institute of Medical Research, Sheba Medical Center, Tel Hashomer 52621, Israel

Received 5 October 2007; accepted 16 September 2008

Abstract

A real-time thermoregulatory model was developed for predicting real-time physiological responses of workers engaged in various tasks for prolonged time. The unique feature of the present model is primarily on metabolic activity inputs derived from minimum non-invasive measures (i.e., heart rate and ambient temperature). In addition, it utilizes individual anthropological characteristics (height, weight, and clothing) as an input to estimate core temperatures (T_c). The model was validated using data from five laboratory studies (n = 63) with varied environments, clothing, and heat acclimation status. Overall, T_c predictions using this simplified model, corresponded well with measured values (root mean square deviation: $0.05-0.31^{\circ}$ C). Published by Elsevier Ltd.

Keywords: Real-time modeling; Heat stress; Heart rate; Core temperature; Air temperature

1. Introduction

Thermoregulatory mathematical models have been increasingly utilized to assess thermal strains of workers without risk, cost, and time related human experiments. Although statistical models limit simulation conditions based on model assumptions, mathematical models consisting of series of thermal physiological equations can provide simulations by generating various combinations of environmental and operational heat stress situations. Previous thermal regulatory models require body core temperature (T_c) as an input [1–3], which is an important physiological parameter for the assessment of thermo physiological strain as it reliably indicates impending injury [4,5]. However, T_c is an invasive measurement and often impractical and undesirable measurement for monitoring during varied activities over prolonged periods in industrial and military situations. In addition, utilizing previous models to predict

physiological responses can be inconvenient and inaccurate for workers, especially soldiers, engaged in various strenuous field activities for prolonged time. For instance, some models can predict physiological responses based on only consistent environmental and operational conditions during work controlled duties [2,3]. Furthermore, many inputs, some of which may be invasive, are required for previous models and tend to provide more inappropriate or missing data in field working environment because strenuous activities in a field are likely to cause sensor malfunctions [1,6]. Therefore, this new suggested model based on a minimum number of non-invasive inputs was needed for predicting real-time physiological responses of soldiers during various prolonged and heat stress related operations. The purpose of this paper is to develop the new model and test the accuracy of the model predictions with a focus on T_c using available data. Although the model in this study was primarily designed for military personnel who are usually heat acclimatized during training with normal or low levels of body fat relative to the general population, the concept of the model can be applicable to industrial and emergency operations.

^{*} Corresponding author. Tel.: +15082335845; fax: +15082335298. E-mail address: Miyo.Yokota@US.ARMY.MIL (M. Yokota).

Comparisons of physiological data with model predictions provide the analytical basis necessary to characterize model performance and, may if necessary, identify areas of further improvements.

2. Methods

The new model represents the human as two active physiological compartments (core and skin) surrounded by a passive clothing compartment. The initial temperature in each compartment was set lower (40.3°C) for heat acclimated individuals [6]. Within a compartment the thermophysiological properties are assumed to be uniform; that is for example, T_c has the same value at time t throughout the core compartment and likewise for skin temperature. All metabolic heat production (M) occurs in the core. Some of the core heat is lost directly to the environment by respiration with the remaining flowing to the skin by conduction and skin blood flow. Overall, the regulation of $T_{\rm c}$ in the model is achieved primarily by controlling blood flow to the skin and sweating rate of the skin. These are reasonable representations and simplifications because of increased blood circulation in warm and hot conditions [6]. The basic thermal regulatory functions including heat production, transfer, balance, and thermal strain index utilized in the model were described below.

2.1. Metabolic rate (M)

A unique feature of this model is the use of real-time estimates of M (Watts) derived from the measured heart rate (HR) and environment temperature [7]. This equation was utilized because the parameters are minimum non-invasive measures and overall good correlation between O_2 uptakes and HR were demonstrated [7,8]. The M equation using HR and environmental temperature was described as follows:

$$M = [0.68 + 4.69(HRratio - 1) - 0.052(HRratio - 1)(T_a - 20)]58.1A_D$$
 (1)

where HRratio—observed HR given at the time/resting HR of the individual, and T_a —ambient temperature in °C. A_D is the body surface area (m²). Cardiac output, indicated by HR, supplies blood and oxygen for metabolism and also blood flow to the skin for thermoregulation. For a given metabolic activity, the HR will increase with increasing environmental temperature because of the thermoregulatory need for increased skin blood flow. The prediction of M shown in Eq. (1) was derived from HR and oxygen consumption measured over a range of metabolic activity and environmental temperature [7]. The equation is tested for the conditions including $20\,^{\circ}\text{C} \leqslant T_a \leqslant 40\,^{\circ}\text{C}$, $1.2 \leqslant \text{HRratio} \leqslant 2.1$, wind speed $\approx 1.25\,\text{m}\,\text{s}^{-1}$, dew point temperature $\leqslant 20\,^{\circ}\text{C}$.

2.2. Heat transfer

Heat exchange from the skin to the environment by radiation and convection is classified as dry heat exchange. The rate of dry heat loss (Q_{dry} , W m⁻²) was determined by

$$Q_{\rm dry}(=T_{\rm sk}-T_{\rm o})/(R_{\rm clt}) \tag{2}$$

where $R_{\rm clt}$ is the total dry thermal resistance between skin and the environment and $T_{\rm o}$ is the operative temperature of the environment [6]. $T_{\rm sk}$ is the skin temperature.

 $R_{\rm clt}$ values for military clothing used in validation process for the present model are from thermal manikin measurements. $T_{\rm o}$ is the average of ambient air $(T_{\rm a})$ and mean radiant temperatures weighted by their respective heat transfer coefficients as described by Kraning and Gonzalez [6].

The evaporative heat loss from the skin (Q_{evap} , W m⁻²) is from water diffusion through the dry skin and from evaporation of areas covered with sweat. It is quantified as [9]:

$$Q_{\text{evap}} = (1 - w)0.06E_{\text{max}} + wE_{\text{max}}$$
 (3)

where the maximum rate of evaporative heat loss from the skin surface ($E_{\rm max}$) completely covered by sweat is calculated from saturated vapor pressure (Torr) of water at the skin temperature, the ambient water vapor pressure (Torr) and the vapor resistance of the clothing system from skin to the surrounding environment. Skin wettedness (w) or the fraction of the skin surface covered by sweat was determined from the rate of sweat secretion to the rate of maximum evaporation from completely wet skin [2].

The heat exchanged via respiration (Q_{res} , W m⁻²) was estimated [9] as

$$Q_{\text{res}} = M/A_D(0.0014(34 - T_a) + 0.0023(44 - P_a)) \tag{4}$$

where P_a is the ambient water vapor pressure (Torr) and T_a is the ambient temperature (${}^{\circ}$ C).

2.3. Heat balance

A heat balance analysis of the core compartment yields,

$$M/A_D = Q_{\text{res}} + Q_k + Q_{\text{skbf}} + (W_{\text{C}}/A_D)c_{\text{bt}}(dT_{\text{c}}/dt)$$
 (5)

where M/A_D is in W m⁻², Q_{res} is respiratory heat loss, Q_k is passive heat conduction from core to the skin, and Q_{skbf} represents heat transported by the blood from core to skin compartments. The last term (dT_c/dt) on the right in Eq. (5) represents the rate of heat storage of the core compartment where W_C is the mass (kg) of the core (≈ 0.95 of total body mass in this case) and specific heat of body tissue (c_{bt}) is 0.97 W h kg⁻¹ °C⁻¹ [2]. The passive heat conduction from core to skin (Q_k) was estimated based on the temperature differences between skin and core and the constant conductance (k) value of the tissue between two compartments (5.28 W m⁻² °C⁻¹) [9]. Similarly, the heat transported by blood flow (Qskbf) to the skin is determined based on skin blood flow, which is modeled proportional to changes in core and skin temperatures from their set point temperatures $(T_{\text{cset}} = 36.8 \,^{\circ}\text{C}; T_{\text{skset}} = 33.7 \,^{\circ}\text{C})$ and specific heat of blood as a constant value of 1.163 W h L⁻¹ $^{\circ}$ C⁻¹ [2]. The rate of T_c ($^{\circ}$ C) change (dT_c/dt) can be rearranged by Eq. (5) to find the next T_c . The energy balance of the skin compartment (W m⁻²) is

Table 1
The summary of three heat study conditions used in this study.

Study#	HS1	HS2	HS3	HS4	HS5
Ta (°C)	27	49	30	35	40
RH (%)	75	18	50	45	40
Acclimation status	No	Yes	Yes	Yes	Yes
Clothing	HWBDU	T-shirt & shorts	HWBDU	CPG	T-shirt & shorts
Activity (W)	277-350	420-620	510-840	~450	~410
Duration (min)	~170	< 100	110	< 40	125
N	9	5	11	8	30
Reference (#)	[11]	[12]	[12]	[13]	[14]

HWBDU-hot weather battle dress uniform and CPG-chemical protective garment.

modeled similarly to T_c substituting the mass (kg) of the skin compartment and T_{sk} , instead [2].

2.4. Physiological strain index (PSI)

The thermal strain index called PSI was utilized based on measured HR and predicted T_c by the model for evaluating online heat strain levels of individuals calculated as follows [10]:

$$PSI = 5(T_{ct} - T_{c0})(39.5 - T_{c})^{-1} + 5(HR_{t} - HR_{0})(180 - HR_{0})^{-1}$$
(6)

where T_{c0} and HR₀ are the initial T_c and HR, respectively. T_{ct} and HR_t are taken at a given time t during the heat exposure [10]. Unlike other thermal indices, PSI is simple, easier to use, and feasible for different operational and environmental conditions [10]. The PSI consists of 0–10 scale, classifying them into five thermal categorical states (no to little, low, moderate, high, very high) [10].

2.5. Validation data

The validation of the model was conducted using data from five different laboratory studies. In all cases, participants provided their informed consent prior to participation and were free to withdraw from the study at any time.

Heat Study 1 (HS1): Nine unacclimated volunteers (8 males, 1 female; age: 23 ± 4 [SD] yr; height 174.2 ± 5.2 cm; weight: 73.4 ± 6.5 kg), wearing the US Army hot weather battle dress uniform (HWBDU) did intermittent exercise in a warm-humid environment (air temperature (T_a) : 27°C, relative humidity (RH): 75%RH) for 170 min [11]. The exercise routine consisted of walking on a level treadmill at 1.34 ms⁻¹ for 30 min followed by 10 min of rest. Grand mean of subjects' HR ranged between 74 and 106 bpm and that of T_c ranged between 37.0 and 37.5°C during the experiment. Rectal temperature was measured each minute [11].

Heat Study 2 (HS2): Five heat acclimated male soldiers (age: $22 \pm 5\,\text{yr}$, height $176 \pm 4\,\text{cm}$; weight: $71.1 \pm 9.3\,\text{kg}$) wearing t-shirt and shorts continuously walked at $420\text{--}620\,\text{W}$ in a hot dry ($49\,^{\circ}\text{C}$, 18%RH) environment [12]. The maximum exercise duration was $100\,\text{min}$ and subjects continued a test session until they voluntary withdrew. Grand mean of subjects' HR

increased from 83 to 157 bpm and that of T_c increased from 36.8 to 38.6 °C during the experiment. T_c was measured with an ingestible telemetry temperature pill [12].

Heat Study 3 (HS3): Eleven volunteers (10 males, 1 female; age: $21\pm8\,\mathrm{yr}$; height: $175\pm7\,\mathrm{cm}$; weight: $78.0\pm11.4\,\mathrm{kg}$), wearing HWBDU, did intermittent exercise in a warm-humid environment (30°C, 50%RH) for 110 min [12]. Subjects are partially heat acclimated by natural summer acclimation but no official acclimation. The exercise routine consisted of walking on a treadmill (1.56 m s⁻¹, 7% grade) for 50 min, followed by 10 min rest. Grand mean of subjects' HR ranged between 82 and 152 bpm and that of $T_{\rm c}$ ranged between 36.8 and 38.2°C during the experiment. Rectal temperature, measured with an ingestible telemetry temperature pill was recorded every 10 min [12].

Heat Study 4 (HS4): Eight heat acclimated men (age: $23 \pm 6\,\mathrm{yr}$; height: $176 \pm 6\,\mathrm{cm}$; weight: $76.0 \pm 15.4\,\mathrm{kg}$), wearing chemical protective garments, walked on a treadmill with a 4–9% grade at $1.56-1.65\,\mathrm{m\,s^{-1}}$ that resulted in metabolic effort about 450W and oxygen uptake around 55% of VO_{2max} until they voluntary withdrew from the study or $T_c > 39.5\,^{\circ}\mathrm{C}$ [13]. Subjects were able to continue exercising for $< 40\,\mathrm{min}$ under environmental conditions of $35\,^{\circ}\mathrm{C}/45\,^{\circ}\mathrm{RH}$. T_c was measured by a rectal probe [13].

Heat Study 5 (HS5): Thirty heat acclimated male volunteers (age: 19 ± 1 yr; height: 180 ± 1 cm; weight: 76.3 ± 2.8 kg) wearing t-shirt and shorts walked on a treadmill at \sim 410 W in the environmental chamber (40°C, 40%RH) for 125 min [14]. Grand mean of subjects' HR increased from 77 to 121 bpm and that of T_c increased from 37.2 and 37.9°C during the experiment. Rectal temperature was measured every minute utilizing a thermistor [14].

Table 1 is the summary of heat study conditions described above. Depending upon the individual study, HR and $T_{\rm c}$ were collected at different time intervals. Previous studies have shown the reliability of swallowed telemetry sensoring to measured $T_{\rm c}$ [15,16].

2.6. Statistical analysis

The predicted and observed T_c for each individual participant were compared using root mean square deviation (RMSD)

method as described in Haslam and Parsons [17]. The RMSD was used to quantify the average difference between predicted and observed measurements across time [17].

3. Results

3.1. Model structure

The concept of the model described above was integrated and the basic operational structure of the new model was summarized in Fig. 1. The model can use individual values, group means or default population values as the input for anthropological characteristics (height, weight, or clothing). Then, real-time input of measured HR and local weather (T_a , wind speed, RH, and radiant load) are used to make predictions and estimates of physiological parameters including T_c , sweat rate, accumulated water loss, $T_{\rm sk}$, metabolism, and thermoregulatory strain [18]. The shaded area indicates an input variable. A box with dotted lines displays multiple functions of the model for predicting outputs (a box with solid lines).

3.2. Validation

Figs. 2–6 summarize the comparisons of the mean measured $T_{\rm c}$ to the corresponding mean model predicted $T_{\rm c}$ using each HS data. Overall, the predictions of $T_{\rm c}$ agreed well with measured values and the RMSD ranged between 0.05 and 0.31 °C.

HS1: In a moderate environment, subjects' T_c were < 37.5 °C and the model predictions were within one SD of the mean measured values (Fig. 2). The mean of one standard deviation (SD) between subjects across the time was 0.19 °C and the prediction errors for HS1 were small (RMSD = 0.10 °C) (Fig. 2).

HS2: Under hot dry environment, mean T_c of volunteers raised ~ 38.5 °C with more variability between subjects across

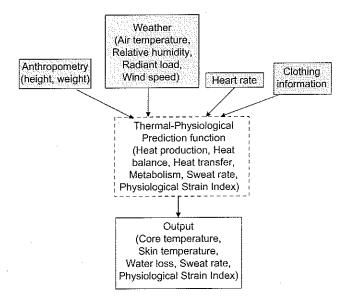


Fig. 1. Basic operational structure of the new model.

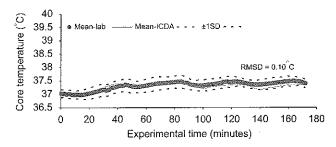


Fig. 2. The summary comparisons between mean measured and predicted core temperature (T_c) from Heat Study 1 (27°C, 75%; hot weather battle dress uniform; n = 9).

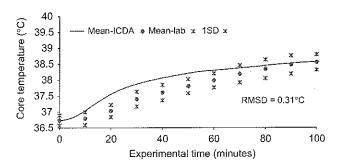


Fig. 3. The summary comparisons between mean measured and predicted core temperature (T_c) from Heat Study 2 (49°C, 18%; t-shirt and shorts; n = 5).

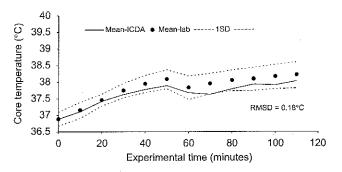


Fig. 4. The summary comparisons between mean measured and predicted core temperature (T_c) from Heat Study 3 (30°C, 50%; hot weather battle dress uniform; n = 11).

the time (0.23 °C) than HS1 (Fig. 3). The RMSD for the model prediction errors was 0.31 °C. Initially, the model predicted a faster rate of increase in $T_{\rm c}$ than measured $T_{\rm c}$ for these heat acclimated participants exercising 49 °C/18%RH. However, the predictions improved after 50 min and were very good deriving the second hour of moderate exercise (Fig. 3).

HS3: During the intermittent exercise in a warm-humid condition, subjects' mean $T_{\rm c}$ increased to 38.2°C. The variability (SD) was also increased from 0.26 to 0.38°C, toward the end of the exercise (Fig. 4). The model prediction followed the patterns of $T_{\rm c}$ responses to intermittent exercise, within 1SD. RMSD was 0.18°C (Fig. 4).

HS4: During the intermittent exercise, subjects' measured mean T_c raised ~38.4°C (Fig. 5). More variability in measured T_c between subjects was observed toward the end of the

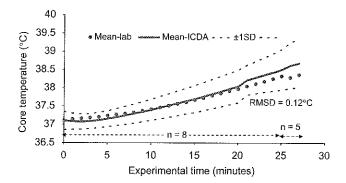


Fig. 5. The summary comparisons between mean measured and predicted core temperature (T_c) from Heat Study 4 (35°C, 45%; protective garment; $n \le 8$).

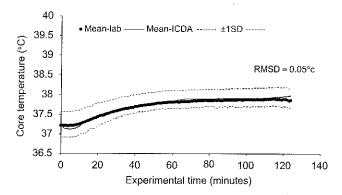


Fig. 6. The summary comparisons between mean measured and predicted core temperature (T_c) from Heat Study 5 (40°C, 40%; t-shirt and shorts; n = 30).

exercise, indicating different physiological responses to heat (Fig. 5). The prediction of T_c in this study agreed with measured values within 1SD, and RMSD for the model prediction errors was relatively small (0.12°C) (Fig. 5).

HS5: Under the operational heat stress (40°C, 40%RH), subjects' mean T_c increased to 37.8°C during the exercise (Fig. 6). The mean of SD between subjects across the time was 0.35°C. T_c predicted by the model agreed well with the measured values and the model prediction errors were very small (RMSD = 0.05°C) (Fig. 6).

4. Discussion

The new model was developed to assist with real-time physiological monitoring of individuals engaged in prolonged work during training or military operations. The initial analysis of the model described in this paper yielded encouraging results for predicting the thermal status of individuals or groups exposed to various heat stress. The model predictions corresponded to the patterns of $T_{\rm c}$ responses to different exercises including intermittent or constant exercise. Predictions for $T_{\rm c}$ were within an acceptable range (\pm 1SD) among five laboratory studies varying different environmental and operational heat stress, acclimation status, and clothing except for a certain exercise period in HS2. Initially, in HS2, the prediction of $T_{\rm c}$ was

conservative in hot dry environment, that is, it tended to increase faster than measured T_c ; however, after approximately sixty minutes, Tc predictions were in good agreement with measured values. This is because of higher HR ratio, resulting into higher M estimates than actual rates, in the beginning. Despite comparing non-compensable heat stress, that occurring with protective clothing (HS4), predictions represented measured T_c fairly well (RMSD = 0.12 °C). Normally, soldiers deploying to regions known for extreme heat will be acclimatized during training for maximizing their performance and prevention from heat-related injuries. As the model based on a minimum number of non-invasive measures was primarily developed for heat acclimated individuals, an acclimatization will provide more accurate predictions of soldiers' physiological status than unacclimated individuals, particularly under strenuous environmental conditions.

The model introduced in this study has an advantage over other heat prediction models in that estimates of M from HR and environmental temperature are obtained using non-invasive methods. Because HR and oxygen consumptions tend to be linearly associated [7,8], HR is useful to estimate metabolic rates. Other methods such as oxygen consumptions and doubly labeled water are alternative to measure metabolic rates; however, they can be destructive, impractical or costly, in prolonged hours of free-range working operations [8]. In addition, invasive measures (e.g., Tc) may interfere with performance and realtime monitoring of soldiers or workers engaged in long hours of training in a wide range of hot environment. The model predicts good agreement with measured T_c , which is useful for screening physiological and health status of workers who may be required to perform different tasks over many hours or even days. This model can provide additional assistance for military operations. For instance, recent reports from Iraq and Afghanistan indicate that faster access to medical care and rapid identification of probable evacuations would save more soldiers' lives [19,20]. One current strategy to shorten the time between injury and treatment is to position a small surgical care unit near the battlefield [19]. The model can contribute to this effort by forecasting both near real-time and the future probability of individual soldier's physiological status and by directing medical attention to the individual soldier, unit medical personnel, or command elements.

There are several programs underway in the Department of Defense to establish methodologies and systems for the accurate "real-time" measurement of physiological status. Although obtaining "true" values of environmental, physiological and operational conditions are desirable for optimum assessment of soldier status, the reality of military operations or other strenuous effort under extreme conditions requires consideration of alternative methods. For instance, the loss of sensor signal, calibration errors, and interference between sensors, are common occurrences resulting in the loss of physiological measurements and accurate health assessments. If model predictions are complicated by the requirements of many physiological, operational, and environmental parameters, the accurate predictions are limited. Strenuous activity may cause sensor malfunction, or make it difficult to repair the device during training or

operational activities. The present model provides a "rugged" alternative to more elaborate sensor suites by utilizing minimum inputs of non-invasive measurements, and can easily be adjusted after sensor loss or to recover data.

This paper has described the promising performance of a new prediction model using laboratory data. However, to further assess model performance, to build user confidence in model predictions, and to identify possible improvements in application and hardware, it is important to test the model during field training involving operational and environmental conditions that are close to operational conditions. Although the present version of our model was created for a specific application using a highly trained, heat acclimated population, the model is readily adaptable to population with variations in fitness, heat acclimation status, body mass, age, or other physical characteristics to extend the model's application to more diverse groups of populations and environments.

5. Summary

A thermal regulatory model was developed for predicting real-time physiological responses of workers engaged in various tasks for prolonged time. The model can use individual values, group means or default population values as the input for anthropological characteristics, real-time input of measured HR and local weather to predict real-time physiological parameters including $T_{\rm c}$, $T_{\rm sk}$, M, water loss, and thermoregulatory strain. The model was validated with various operational (e.g., clothing, activities, acclimation status) and environmental (e.g., 27–49 °C) conditions from five laboratory heat studies (n=63). The $T_{\rm c}$ predictions were overall in good agreement (RMSD: 0.05–0.31 °C) with measured core temperatures.

Conflict of interest statement

None.

Disclaimer

The investigators have adhered to the policies for protection of human subjects as prescribed in Army Regulation 70–25, and the research was conducted in adherence with the provisions of 32 CFR Part 219. The opinions or assertions contained herein are the private views of the author(s) and are not to be construed as official or as reflecting the views of the Army or the Department of Defense.

References

- K.K. Kraning, R.R. Gonzalez, A mechanistic computer simulation of human work in heat that accounts for physical and physiological effects of clothing, aerobic fitness, and progressive dehydration, J. Therm. Biol. 22 (1997) 331–342.
- [2] A.P. Gagge, A.P. Fobelets, L.G. Berglund, A standard predictive index of human response to the thermal environment, ASHRAE Trans. 92 (1986) 709-731.
- [3] K.B. Pandolf, L.A. Stroschen, L.L. Drolet, et al., Prediction modeling of physiological responses and human performance in the heat, Comput. Biol. Med. 16 (1986) 319–329.

- [4] D. Amos, R. Hansen, W.M. Lau, et al., Physiological and cognitive performance of Soldiers conducting routine patrol and reconnaissance operations in the tropics, Mil. Med. 165 (2000) 961–966.
- [5] K.B. Pandolf, R.F. Goldman, Convergence of skin and rectal temperatures as a criterion for heat tolerance, Aviat. Space Environ. Med. 49 (1978) 1095-1101.
- [6] K.K. Kraning, R.R. Gonzalez, Physiological consequences of intermittent exercise during compensable and uncompensable heat stress, J. Appl. Physiol. 71 (1991) 2138–2145.
- [7] L.G. Berglund, Heart rate as an indicator of metabolic rate in hot environments, in: Alliance for Engineering in Medicine and Biology, Proceedings of 30th Annual Conference on Engineering in Medicine and Biology, 19, 1977, Los Angeles, CA, Arlington, VA, November 5-9, 1977, pp. 274.
- [8] W.D. McArdle, F.I. Katch, V.L. Katch, Human energy expenditure during rest and physical activity, in: W.D. McArdle, F.I. Katch, V.L. Katch (Eds.), Exercise Physiology: Energy, Nutrition and Human Performance, Lippicott Williams and Wilkins, Baltimore, 1996, pp. 150-165.
- [9] P.O. Fanger, Thermal Comfort, MacGraw-Hill, New York, 1972.
- [10] D.S. Moran, A. Shitzer, K.B. Pnadolf, A physiological strain index to evaluate heat stress, Am. J. Physiol. 275 (1998) R129-R134.
- [11] W.R. Santee, L.G. Berglund, A. Cardello, et al., Physiological and comfort assessment of volunteers wearing Battle Dress Uniforms (BDU) of different fabrics during intermittent exercise, Technical Report T06-06, US Army Research Institute of Environmental Medicine, MA, 2006
- [12] S.N. Cheuvront, S.J. Montain, D.A. Goodman, et al., Evaluation of the limits to accurate sweat loss prediction during prolonged exercise, Eur. J. Appl. Physiol. 101 (2007) 215–224.
- [13] W.A. Latzka, M.N. Sawka, S.J. Montain, et al., Hyperhydration: tolerance and cardiovascular effects during uncompensable exercise-heat stress, J. Appl. Physiol. 84 (1998) 1858–1864.
- [14] D.S. Morán, Y. Heled, L. Still, et al., Assessment of heat tolerance for post exertional heat stroke individuals, Med. Sci. Monit. 10 (2004) CR252-CR257.
- [15] M.A. Kolka, M.D. Quigley, L.A. Blanchard, et al., Validation of a temperature telemetry system during moderate and strenuous exercise, J. Therm. Biol. 18 (1993) 203-211.
- [16] C. O'Brien, R.W. Hoyt, M.J. Buller, et al., Telemetry pill measurement of core temperature in human during active heating and cooling, Med. Sci. Sports Exerc. 30 (1998) 468–472.
- [17] P.A. Haslam, K.C. Parsons, An evaluation of computer-based models that predict human responses to the thermal environment, ASHRAE Trans. 94 (1998) 1342-1360.
- [18] M. Yokota, L.G. Berglund, Initial capability decision aid (ICDA) thermal and its validation, Technical Report T06-03, US Army Research Institute of Environmental Medicine, Massachusetts, 2006.
- [19] T.R. Bilski, B.C. Baker, J.R. Grove, R.P. Hinks, Battlefield casualties treated at Camp Rhino, Afghanistan: lessons learned, J. Trauma 54 (2003) 814–822.
- [20] A. Gawande, Casualties of war—military care for the wounded from Iraq and Afghanistan, N. Engl. J. Med. 351 (2004) 2471-2475.

Miyo Yokota received her B.A. (1988) from Kyoto Women's University in Japan, M.A. from Western Michigan University (1991), and Ph.D. in Biological Anthropology from University of Tennessee, Knoxville, in 1997. Currently, she is a Senior National Research Council Associate in Biophysics and Biomedical Modeling Division, US Army Research Institute of Environmental Medicine, Natick, MA. Her research interests include human variability in body composition and thermal regulatory modeling.

Larry G. Berglund is a registered Professional Mechanical, Electrical, and Bioenvironmental Engineer by education (University of Minnesota (B.S., M.S.), University of New Haven (B.S.), Kansas State University (Ph.D.)). His professional career includes Trane Company, Michigan Technological University, Pierce Foundation Laboratory/Yale University, Tohoku University (Japan), and Kimberly Clark Corporation before joining US Army Research Institute of Environmental Medicine in 2000. His focus is on applications of bio-thermal modeling.

Samuel Cheuvront received degrees in Nutrition from Indiana University of Pennsylvania, USA, in 1994 and 1996, and a Ph.D. in exercise physiology from Florida State University in 2000. From 2000 to 2003, Dr. Cheuvront completed a Post Doc in Environmental Physiology at the US Army Research Institute of Environmental Medicine (USARIEM) where he remains currently as a Principal Investigator. His research centers around the study of environmental and nutritional influences on Soldier performance.

William Santee received a B.A. degree from Gustavus Adolphus College in 1970, an MS from the University of Georgia in 1978, and a Ph.D. from Indiana State University in 1985. He has been at The US Army Research Institute of Environmental Medicine since 1985, where he is a Research Physical Scientist in the Biophysics and Biomedical Modeling Division. His research interests focus on biometeorology and the biophysics of human heat exchange.

William Latzka received B.S. degrees in Biology and Health and a M.S. in Exercise Physiology from St. Cloud State University, Minnesota, USA, in 1980 and 1982, and a Sc.D. in Applied Physiology from Boston University in 1996. From 1996 to 2001, Dr. Latzka completed a Post Doc in Environmental Physiology at the US Army Research Institute of Environmental Medicine (USARIEM) where he is currently the Chief of Research Support Division/Executive Officer. His research interests focused on improving Soldier performance in extreme environments.

Scott Montain received a B.S. degree from the University of Wisconsin-LaCrosse, USA in 1981 and a Ph.D., from The University of Texas at Austin, USA, in 1991. Since 1991, he has been with the US Army Research Institute of Environmental Medicine, Natick, MA, USA where he is a Research Physiologist in the Military Nutrition Division. His research focuses on nutritional strategies to sustain performance during environmental stress.

Margaret Kolka received her B.S. (1974) and M.A. (1976) degrees from Michigan State University and her Ph.D. in Exercise Physiology in 1980 from Indiana University. She joined Thermal Physiology Division, US Army Research Institute of Environmental Medicine (USARIEM), Natick, MA as a Research Physiologist in 1983 and was Chief, Biophysics and Biomedical Modeling Division, USARIEM, from 2004–2005.

Daniel Moran received his Ph.D. (hon.) from the Sackler School of Medicine in Tel Aviv University (Israel) in 1993. Since 1990, he has been with the Heller Institute of Medical Research, where he acts as the Director from 2000. His research interests focus on physiological evaluation of human performance during various environments and stresses, non-invasive methods for physiological monitoring, and biomarkers of bone-remodeling.